# **Spaceflight Mechanics**

#### **Exercise set 7**

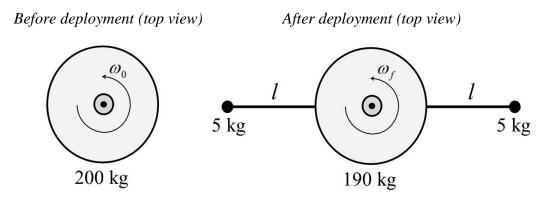
**1.** A cylindrical, homogeneous satellite has mass of 200 kg, radius 1 m, and height 0.5 m. Its orientation is associated with the following Euler parameters (quaternions):

$$q_0 = 0.5$$
  $q_1 = 0.75$   $q_2 = \frac{\sqrt{3}}{4}$   $q_3 = 0$ 

(a) Obtain the Bryant's angles (sequence 3-2-1) associated with this orientation.

The satellite has pure spin about the axis of maximal inertia, with angular rate  $\omega_0 = 3 \text{ sec}^{-1}$ . Then, two appendices are deployed. They are modeled as point masses, and each of them has mass of 5 kg (see figure, taken from the top). The rods that connect these two masses with the cylinder are rigid and massless. After deployment, the angular rate decreases to  $\omega_f = 1 \text{ sec}^{-1}$ .

(b) Calculate the length of each rod (denoted with *l* in the figure).



2. An axisymmetric satellite, with symmetry axis  $\hat{e}_3$ , is not subject to external torques and no energy dissipation occurs. At a given time  $t_0$ , the satellite rotates with angular velocity components given by

 $\omega_{10} = 0.02 \text{ sec}^{-1}$   $\omega_{20} = -0.05 \text{ sec}^{-1}$   $\omega_{30} = 0.5 \text{ sec}^{-1}$ 

whereas the principal inertia moments are

$$I_1 = I_2 = I_T = 200 \text{ kg} \cdot \text{m}^2$$
  $I_3 = 250 \text{ kg} \cdot \text{m}^2$ 

The inertial axis  $\hat{E}_3$  is aligned with the angular momentum  $H_c$ , and the Euler angles (sequence 3-1-3) are employed to describe the instantaneous spacecraft orientation. The precession angle  $\psi$  at  $t_0$  equals 60 deg.

- (a) Calculate the angular momentum components along the principal axes of inertia at  $t_0$ .
- (**b**) Evaluate the nutation angle  $\theta$  and the spin angle  $\phi$  at  $t_0$ .
- (c) At  $t_0$ , obtain the rotation matrix  $\underset{B \leftarrow I}{\mathbf{R}}$ , where B  $(\hat{e}_1, \hat{e}_2, \hat{e}_3)$  is the reference frame associated with the principal axes of inertia and I  $(\hat{E}_1, \hat{E}_2, \hat{E}_3)$  is the inertial frame.

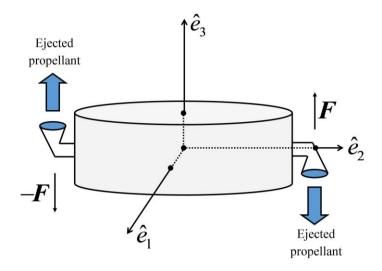
At  $t_0 + 60$  sec, an impulsive torque (with duration of 1 sec) is applied, such that the subsequent attitude motion is pure spin about body axis  $\hat{e}_3$ .

- (d) Determine direction (in the body axes frame  $(\hat{e}_1, \hat{e}_2, \hat{e}_3)$ ) and magnitude of this impulsive torque.
- 3. A cylindrical axisymmetric spacecraft has radius of 1 m, moments of inertia

 $I_1 = I_2 = I_T = 20 \text{ kg} \cdot \text{m}^2$   $I_3 = 35 \text{ kg} \cdot \text{m}^2$ 

and is subject to no external torque. Axis  $\hat{E}_3$  of the inertial reference frame is aligned with the angular momentum  $H_C(t_0^-)$ ; the spacecraft rotates with a constant nutation angle  $\theta$  of 60 deg and a transverse velocity component  $\omega_{12} = \sqrt{\omega_1^2 + \omega_2^2} = 0.3 \text{ sec}^{-1}$ . At  $t_0^ \omega_1(t_0^-) = -\omega_{12}$ .

- (a) Determine the angular velocity component  $\omega_3$ .
- (b) The spacecraft is equipped with two thrusters (see figure below), which are ignited for 1 sec at  $t_0$  and provide a propulsive thrust F, whose magnitude F equals 1 newton. Under the impulsive torque assumption, obtain the components (along the body axes) of the angular momentum  $H_C(t_0^+)$  after ignition of the two thrusters.
- (c) A new inertial reference frame is defined, with axis  $\hat{E}'_3$  aligned with  $H_C(t_0^+)$ . Calculate the nutation angle at  $t_0^+$ , with respect to  $\hat{E}'_3$ .
- (d) In the new inertial reference frame, the precession angle at  $t_0^+$  is  $\psi(t_0^+) = 0$ . Determine the principal axis and angle associated with the instantaneous orientation of the spacecraft at time  $t = t_0 + 60$  sec.



4. An axisymmetric satellite, with symmetry axis  $\hat{e}_3$  aligned with the satellite longitudinal axis, is not subject to external torques and no energy dissipation occurs. At a given time  $t_0$ , the satellite rotates with angular velocity components given by

 $\omega_{10} = -0.05 \text{ sec}^{-1}$   $\omega_{20} = 0.02 \text{ sec}^{-1}$   $\omega_{30} = 0.5 \text{ sec}^{-1}$ 

whereas the principal inertia moments are

$$I_1 = I_2 = I_T = 100 \text{ kg} \cdot \text{m}^2$$
  $I_3 = 150 \text{ kg} \cdot \text{m}^2$ 

The inertial axis  $\hat{E}_3$  is aligned with the angular momentum  $H_c$ , and the Euler angles (sequence 3-1-3) are employed to describe the instantaneous spacecraft orientation. The precession angle  $\psi$  at  $t_0$  equals 30 deg.

- (a) Calculate the angular momentum components along the principal axes of inertia at  $t_0$
- (**b**) Evaluate the nutation angle  $\theta$  and the spin angle  $\phi$  at  $t_0$
- (c) At  $t_0$ , obtain the rotation matrix  $\underset{B \leftarrow I}{\mathbf{R}}$ , where B  $(\hat{e}_1, \hat{e}_2, \hat{e}_3)$  is the reference frame associated with the principal axes of inertia and I  $(\hat{E}_1, \hat{E}_2, \hat{E}_3)$  is the inertial frame.

## **SOLUTION OF EXERCISE 1**

**Point** (a). The rotation matrix associated with the instantaneous orientation is found on the basis of the known values of quaternions,

$$\mathbf{R}_{B\leftarrow I} = \begin{bmatrix} q_0^2 + q_1^2 - q_2^2 - q_3^2 & 2(q_1q_2 + q_0q_3) & 2(q_1q_3 - q_0q_2) \\ 2(q_1q_2 - q_0q_3) & q_0^2 + q_2^2 - q_1^2 - q_3^2 & 2(q_2q_3 + q_0q_1) \\ 2(q_1q_3 + q_0q_2) & 2(q_2q_3 - q_0q_1) & q_0^2 + q_3^2 - q_2^2 - q_1^2 \end{bmatrix} = \begin{bmatrix} 0.6250 & 0.6495 & -0.4330 \\ 0.6495 & -0.1250 & 0.7500 \\ 0.4330 & -0.7500 & -0.5000 \end{bmatrix}$$

Then, Bryant's angles are found from the general relations that yield them from  $\underset{B \leftarrow I}{\mathbf{R}}$ 

$$\theta = -\arcsin r_{13} = 25.66 \deg$$

$$\sin\psi = \frac{r_{12}}{\cos\theta} = 0.7206 \text{ and } \cos\psi = \frac{r_{11}}{\cos\theta} = 0.6934 \implies \psi = 2\arctan\frac{0.7206}{1+0.6934} = 46.10 \text{ deg}$$
$$\sin\phi = \frac{r_{23}}{\cos\theta} = 0.8321 \text{ and } \cos\phi = \frac{r_{33}}{\cos\theta} = -0.5527 \implies \phi = 2\arctan\frac{0.8321}{1-0.5527} = 123.69 \text{ deg}$$

where  $\{r_{ij}\}$  are the elements of matrix  $\mathbf{R}_{B\leftarrow I}$ .

**Point** (b). As a first step, using the relations that hold for a homogeneous cylinder, the principal moments of inertia are

$$I_3 = \frac{MR^2}{2} = 100 \text{ kg m}^2$$
  $I_1 = I_2 = \frac{M}{12} (3R^2 + H^2) = 54.167 \text{ kg m}^2$ 

Hence, the axis of maximal inertia is  $\hat{e}_3$  and pure spin occurs about this axis. Due to conservation of the angular momentum,

$$I_{3}^{-}\omega_{0} = \left[I_{3}^{+} + 2\tilde{m}(l+R)^{2}\right]\omega_{f} \quad \text{where}$$
$$I_{3}^{-} = I_{3} = 100 \text{ kg m}^{2} \quad I_{3}^{+} = \frac{M_{f}R^{2}}{2} = 95 \text{ kg m}^{2} \quad \left(M_{f} = 190 \text{ kg}\right) \quad \tilde{m} = 5 \text{ kg}$$

Hence, one obtains

$$(l+R)^2 = \frac{I_3^- \omega_0 - I_3^+ \omega_f}{2\tilde{m}\omega_f} \implies l = 3.528 \text{ m}$$

#### **SOLUTION OF EXERCISE 2**

**Point** (a). The three components  $(\hat{e}_1, \hat{e}_2, \hat{e}_3)$  of the angular momentum  $H_c$  are

$$H_1 = I_1 \omega_{10} = 4 \text{ kg } \frac{\text{m}^2}{\text{sec}}$$
  $H_2 = I_2 \omega_{20} = -10 \text{ kg } \frac{\text{m}^2}{\text{sec}}$   $H_3 = I_3 \omega_{30} = 125 \text{ kg } \frac{\text{m}^2}{\text{sec}}$ 

**Point** (b). Because  $\hat{E}_3$  is aligned with the angular momentum  $H_c$ , the spin angle  $\phi_0$  and the nutation angle  $\theta_0$  are given by

$$\theta_0 = \arccos\left[\frac{H_3}{H_c}\right] \qquad \left(H_c = |\boldsymbol{H}_c|\right) \implies \theta_0 = 4.9 \text{ deg}$$
$$\sin \phi_0 = \frac{H_1}{H_c \sin \theta_0} \quad \text{and} \quad \cos \phi_0 = \frac{H_2}{H_c \sin \theta_0} \implies \phi_0 = 158.2 \text{ deg}$$

**Point** (c). The rotation matrix  $\underset{B \leftarrow I}{\mathbf{R}}$  is found as the result of three consecutive elementary rotations,

$$\mathbf{R}_{B \leftarrow I} = \mathbf{R}_{3}(\phi_{0})\mathbf{R}_{1}(\theta_{0})\mathbf{R}_{3}(\psi_{0}) = \begin{bmatrix} -0.7847 & -0.6191 & 0.0319 \\ 0.6154 & -0.7842 & -0.0797 \\ 0.0743 & -0.0429 & 0.9963 \end{bmatrix}$$

**Point (d)**. An axisymmetric satellite rotates with angular velocity components (along  $(\hat{e}_1, \hat{e}_2, \hat{e}_3)$ ) given by

$$\omega_1 = \omega_{12} \cos(\omega_P t + \varphi)$$
  $\omega_2 = \omega_{12} \sin(\omega_P t + \varphi)$   $\omega_3 = \omega_{30}$ 

where

$$\omega_{12} = \sqrt{\omega_{10}^2 + \omega_{20}^2} \qquad \omega_P = \omega_{30} \left( \frac{I_3}{I_T} - 1 \right) \qquad \sin \varphi = \frac{\omega_{20}}{\omega_{12}} \qquad \cos \varphi = \frac{\omega_{10}}{\omega_{12}}$$

After 60 sec, one obtains the following values for the angular velocity components (at  $t_1 = t_0 + 60$  sec):

$$\omega_1(t_1) = 0.0538 \text{ sec}^{-1}$$
  $\omega_2(t_1) = 0.0014 \text{ sec}^{-1}$   $\omega_3(t_1) = 0.5 \text{ sec}^{-1}$ 

and the corresponding components of the angular momentum are given by

$$H_1(t_1) = I_1\omega_1(t_1)$$
  $H_2(t_1) = I_2\omega_2(t_1)$   $H_3(t_1) = I_3\omega_3(t_1)$ 

Right after the impulsive torque (at  $t_1^+$ ), the satellite rotates with pure spin about axis 3, therefore the components of  $H_c$  are

$$H_1(t_1^+) = 0$$
  $H_2(t_1^+) = 0$   $H_3(t_1^+) = I_3\omega_3(t_1)$ 

This means that

$$\boldsymbol{H}_{C}\left(\boldsymbol{t}_{1}^{+}\right) - \boldsymbol{H}_{C}\left(\boldsymbol{t}_{1}\right) = \boldsymbol{L}_{C}\Delta t \qquad \left(\Delta t = 1 \text{ sec}\right)$$

and finally one obtains the three torque components

$$L_{c1} = \frac{H_1(t_1^+) - H_1(t_1)}{\Delta t} = -10.7665 \text{ N m}$$
$$L_{c2} = \frac{H_2(t_1^+) - H_2(t_1)}{\Delta t} = -0.2856 \text{ N m}$$
$$L_{c3} = \frac{H_3(t_1^+) - H_3(t_1)}{\Delta t} = 0 \text{ N m}$$

and the torque magnitude

$$L_c = 10.7703 \text{ N m}$$

## **SOLUTION OF EXERCISE 3**

**Point (a).** For free-torque motion of an axisymmetric spacecraft, if  $\hat{E}_3$  is aligned with the angular momentum, then the angular velocity component  $\omega_3$  and the transverse angular velocity  $\omega_{12}$  fulfill the following relation:

$$\frac{I_T \omega_{12}}{I_3 \omega_3} = \tan \theta \quad \rightarrow \quad \omega_3 = \frac{I_T \omega_{12}}{I_3 \tan \theta} = 0.099 \text{ sec}^{-1}$$

**Point (b)**. The two thrusters portrayed in the figure provide a torque  $L_c$  aligned with body axis  $\hat{e}_1$ , i.e.  $L_c = L_{c1}\hat{e}_1$ . The torque component  $L_{c1}$  is given by

$$L_{c_1} = 2FR = 2$$
 N m

This torque is applied for 1 sec, hence its action can be approximated as instantaneous (impulsive torque assumption). The angular momentum variation at  $t_0$  is given by

$$\boldsymbol{H}_{C}\left(\boldsymbol{t}_{0}^{+}\right) - \boldsymbol{H}_{C}\left(\boldsymbol{t}_{0}^{-}\right) = \boldsymbol{L}_{C}\Delta t \qquad \left(\Delta t = 1 \text{ sec}\right)$$

As a result, right after the impulse, the angular momentum is

$$\boldsymbol{H}_{C}(t_{0}^{+}) = \begin{bmatrix} -4 & 0 & 3.464 \end{bmatrix} \begin{bmatrix} \hat{e}_{1} \\ \hat{e}_{2} \\ \hat{e}_{3} \end{bmatrix} \operatorname{kg} \frac{\mathrm{m}^{2}}{\mathrm{sec}} \quad \text{i.e.} \quad \begin{cases} H_{C1} = -4 \, \operatorname{kg} \, \mathrm{m}^{2} / \mathrm{sec} \\ H_{C2} = 0 \\ H_{C3} = 3.464 \, \operatorname{kg} \, \mathrm{m}^{2} / \mathrm{sec} \end{cases}$$

**Point** (c). At  $t_0^+$ , because  $\hat{E}_3'$  is aligned with  $H_C(t_0^+)$ , the following relations hold:

$$\cos\left[\theta\left(t_{0}^{+}\right)\right] = \frac{I_{3}\omega_{3}\left(t_{0}^{+}\right)}{H_{c}\left(t_{0}^{+}\right)} \longrightarrow \theta\left(t_{0}^{+}\right) = 49.1 \text{ deg}$$

$$\begin{cases} \sin\left[\phi\left(t_{0}^{+}\right)\right] = \frac{I_{T}\omega_{1}\left(t_{0}^{+}\right)}{H_{c}\left(t_{0}^{+}\right)\sin\left[\theta\left(t_{0}^{+}\right)\right]} \longrightarrow \phi\left(t_{0}^{+}\right) = -90 \text{ deg} \end{cases}$$

$$\cos\left[\phi\left(t_{0}^{+}\right)\right] = \frac{I_{T}\omega_{2}\left(t_{0}^{+}\right)}{H_{c}\left(t_{0}^{+}\right)\sin\left[\theta\left(t_{0}^{+}\right)\right]} \longrightarrow \phi\left(t_{0}^{+}\right) = -90 \text{ deg} \end{cases}$$

Point (d). The time evolution of the three Euler angles for an axisymmetric spacecraft is

$$\psi(t) = \psi(t_0^+) + \frac{\omega_{12}}{\sin \theta}(t - t_0)$$
  

$$\theta(t) = \theta(t_0^+)$$
  

$$\phi(t) = \phi(t_0^+) + \omega_3(t_0^+) \left[1 - \frac{I_3}{I_T}\right](t - t_0)$$

Right after the impulsive torque the angular velocity components are

$$\omega_1(t_0^+) = \frac{H_{C1}}{I_T} = -0.2 \operatorname{sec}^{-1} \qquad \omega_1(t_0^+) = \frac{H_{C2}}{I_T} = 0 \qquad \omega_3(t_0^+) = \frac{H_{C3}}{I_3} = 0.099 \operatorname{sec}^{-1}$$

Hence, at time  $\overline{t} = t_0 + 60 \text{ sec}$ , the three Euler angles equal

$$\psi(\overline{t}) = 189.5 \text{ deg}$$
  $\theta(\overline{t}) = 49.1 \text{ deg}$   $\phi(\overline{t}) = 14.8 \text{ deg}$ 

At  $\overline{t}$  the rotation matrix  $\underset{B\leftarrow I}{\mathbf{R}}$  is the result of three subsequent elementary rotations 3-1-3 by angles  $\psi(\overline{t})$ ,  $\theta(\overline{t})$ , and  $\phi(\overline{t})$ . The general expression derived during the lectures can be used, to obtain

$$\mathbf{R}_{B\leftarrow I} = \begin{bmatrix} -0.9256 & -0.3253 & 0.1933 \\ 0.3571 & -0.5818 & 0.7308 \\ -0.1253 & 0.7455 & 0.6547 \end{bmatrix}$$

Once the rotation matrix is found, the principal axis and angle can be derived,

$$\Phi = \arccos\left\{\frac{1}{2}\left[r_{11} + r_{22} + r_{33} - 1\right]\right\} = 157.9 \text{ deg}$$

$$a_{1} = \frac{r_{23} - r_{32}}{2\sin\Phi} = -0.0195$$

$$a_{2} = \frac{r_{31} - r_{13}}{2\sin\Phi} = -0.4230$$

$$a_{3} = \frac{r_{12} - r_{21}}{2\sin\Phi} = -0.9059$$

where  $\{r_{ij}\}$  are the elements of matrix  $\mathbf{R}_{B \leftarrow I}$ .

### **SOLUTION OF EXERCISE 4**

**Point** (a). The three components of the angular momentum (along the principal axes of inertia) are

$$H_1 = I_1 \omega_{10} = -5 \text{ kg} \cdot \frac{\text{m}^2}{\text{sec}}$$
  $H_2 = I_2 \omega_{20} = 2 \text{ kg} \cdot \frac{\text{m}^2}{\text{sec}}$   $H_3 = I_3 \omega_{30} = 75 \text{ kg} \cdot \frac{\text{m}^2}{\text{sec}}$ 

**Point** (b). When  $\hat{E}_3$  is aligned with  $H_c$ , the following relations hold:

$$\cos\theta_0 = \frac{I_3\omega_{30}}{H_c} \qquad \sin\phi_0 = \frac{I_1\omega_{10}}{H_c\sin\theta_0} \qquad \cos\phi_0 = \frac{I_2\omega_{20}}{H_c\sin\theta_0}$$

and lead to obtaining the desired values

 $\theta_0 = 4.1 \text{ deg}$  and  $\phi_0 = -68.2 \text{ deg}$ 

**Point** (c). At  $t_0$  the rotation matrix  $\underset{B \leftarrow I}{\mathbf{R}}$  is the result of three subsequent elementary rotations 3-1-3 by angles  $\psi_0$ ,  $\theta_0$ , and  $\phi_0$  (the Euler angles). The general expression derived during the lectures can be used, to obtain

$$\mathbf{R}_{B\leftarrow I} = \begin{bmatrix} 0.7847 & -0.6163 & -0.0665 \\ 0.6189 & 0.7850 & 0.0266 \\ 0.0358 & -0.0620 & 0.9974 \end{bmatrix}$$